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Process for producing rutile TiO₂ by oxidation of TiCl₄ in the presence of PCl₃ and AlCl₃

The present invention relates to a process for preparing titanium dioxide from titanium tetrachloride, aluminum trichloride and phosphorous trichloride by oxidation. More specifically, the process of the present invention relates to preparing titanium dioxide by oxidation of titanium tetrachloride in the presence of aluminum chloride followed by the addition of phosphorous trichloride when the conversion to titanium dioxide is at least 80%.

It is disclosed in U.S. Patent 3,547,671 that titanium tetrachloride can be oxidized in the presence of aluminum trichloride and phosphorous trichloride to give rutile titanium dioxide. The amount of AlCl₃ was sufficient to form 2—4% Al₂O₃ and the amount of PCl₃ was sufficient to form from 0.5—3% P₂O₅ based on the weight of TiO₂ pigment formed. It is also disclosed that rutilization is impeded by PCl₃ but that the effect of PCl₃ may be compensated for by increasing the AlCl₃.

Now a process has been found for preparing titanium dioxide substantially in the rutile form. The present invention provides for obtaining a higher rutile TiO2 at any given level of AICI3 within the scope of the invention as compared to simultaneous addition of AICl₃ and PCl₃ at one point in the reaction. The process of this invention comprises the oxidation of TiCl₄, in the presence of AICl₃, with the later introduction into the oxidation of PCl₃, when at least 80% of the TiCl₄ is converted to TiO₂.

According to the present invention, there is provided a process for the manufacture of TiO₂

essentially in the rutile form by reacting TiCl4 and oxygen or an oxygen containing gas in a reaction chamber in the presence of AlCl₃ and PCl₃ characterised in that the AlCl₃ and PCl₃ are separately introduced in an amount which is such as to provide from 0.1 to 0.5% by weight P₂O₅ and from 0.1 to 1.5% by weight Al₂O₃, calculated on the weight of the final TiO₂ pigment and in that the PCl₃ is added after the AlCl₃ addition and at a stage in the process where TiCl₄ is at least 80% converted to TiO₂. The oxidation is conducted in the presence of oxygen or a gas containing oxygen. The oxygen or gas containing oxygen is in general preheated to a temperature of 800—1600°C and then is normally introduced into a reaction chamber of a metal pipeline-type reactor. The temperature in the reactor of

introduced into a reaction chamber of a metal pipeline-type reactor. The temperature in the reactor of the combined oxidizing gas stream and TiCl₄/AlCl₃ can range rather widely. Generally, the temperature ranges from 1000-1500°C.

Aluminum trichloride is in practice added with the titanium tetrachloride in such a manner that the aluminum trichloride and titanium tetrachloride are uniformly distributed into the reactor space so that more efficient contact with preheated oxygen occurs. The aluminum trichloride and titanium tetrachloride may be mixed and then sprayed concentrically in the vapor state into the reactor. Rapid, efficient mixing of the TiCl₄/AlCl₃ can be accomplished by the use of an annular ring with outlets and side tee mixing, as taught in U.S. Patent 2,791,490, and this is preferred.

An amount of aluminum trichloride can be added which is sufficient to form 0.1—1.5% Al₂O₃ based on the TiO₂ pigment. Amounts of AlCl₃ that will form less than 0.1% will give optical values for the product TiO₂ that are lower to the point of making a less efficient pigment. Amounts of AlCl₃ that will form more than 1.5% Al₂O₃ can be used with no advantage. Minimization of the AICl₃ reduces corrosion of the metallic reactor. However, AICl₃ is essential in the formation of rutile TiO₂. Corrosion of the metallic reactor that results with oxidation in the presence of AICI3, PCI3, TiCl4 is greatly reduced by the present invention.

Phosphorous trichloride is added to the reactor at a point in the oxidation reaction where at least 80%, preferably 88—98%, more preferably 90—94%, of the TiCl, introduced into the reactor has been converted to TiO2. In a pipeline-type reactor, the addition point of PCI3 will vary depending on the size of the reactor and the particular target conversion level. For example in the case of a 10-inch (254 mm) inside diameter tubular reactor with oxygen at 980°C and operating at a rate of 7830 kg of oxygen per hour with sufficient Al_2O_3 to provide 1% Al_2O_3 in the TiO_2 it was determined that at a point 5 feet (1.52 metre) from the entrance of the $TiCl_4$ a conversion of 92% of the $TiCl_4$ to TiO_2 had occurred so that PCl_3 addition conveniently could be effected at this point.

The reaction initiated is an exothermic type. Therefore, the temperature in the reactor is generally at least 800°C and in general ranges from 800—1500°C and preferably 1100—1500°C. The addition of the PCI3 after the achievement of at least 80% conversion to TiO2, results in the need for less AICI3 to achieve the levels of rutilization achieved by this invention. Thus, the present invention offers better control of rutilization. The percent rutile in the product TiO₂ achieved by this invention is generally from 85—100%, preferably 92—100% and most preferably 98—100%. The present process can produce more rutile at a given level of AlCl, than does the process where the addition of AICI₃ and PCI₃ take place at the same point in the reaction. Percent rutile is determined by X-ray diffraction as is well known in the art.

Thus, the present invention enables better control of rutilization and reduced corrosion of the metallic reactor through reduced levels of AICI3 with the capability of achieving essentially complete rutilization. What is meant by essentially complete rutilization is 98-100%.

The amount of PCl₃ that is added in the process of this invention is sufficient to form 0.1—0.5% P_2O_5 , preferably 0.1—0.3% P_2O_5 in the TiO₂. Amounts of PCl₃ that will form less than 0.1% P_2O_5 result in lower optical values for the TiO₂. Amounts of PCl₃ that will form more than 0.5% P_2O_5 give no

advantage. When PCl_3 is added with $AlCl_3$ and $TiCl_4$, the rutilization, among other things, is effected. More $AlCl_3$ is therefore required. However, when PCl_3 is added after the $TiCl_4$ / $AlCl_3$ addition and after at least 80% of the $TiCl_4$ is converted to TiO_2 , the PCl_3 does not substantially affect the rutilization and therefore less $AlCl_3$ is required to achieve a given rutilization.

The process of this invention also results in a reduction in the viscosity of a slurry of the ${\rm TiO_2}$ in the processing of the ${\rm TiO_2}$ product. The ${\rm TiO_2}$ resulting from the oxidation reaction of this invention is in a semi-finished state. In order to prepare the ${\rm TiO_2}$ for use in paper and board applications, a slurry is prepared as is illustrated in Example 3 below. In paint and plastics use the ${\rm TiO_2}$ is wet treated, washed and milled to a dry powder.

Examples

In the examples that follow all percentages and parts are by weight unless otherwise indicated.

Example 1—(best mode)

A stream of oxygen preheated to a temperature of 980°C was introduced into one end of a 10-inch (254 mm) inside diameter tubular, chlorine-purged reactor operated at 1.76 kg/cm² (280.6 kPa) gauge at a rate of 7730 kg per hour.

A titanium tetrachloride stream containing sufficient aluminum trichloride to provide one percent Al₂O₃ in the titanium dioxide based on the titanium dioxide was preheated to 480°C and introduced into the reactor in vapor form through an annular ring and mixing tee to ensure complete and uniform mixing with the preheated oxygen.

The temperature of the reaction gas stream was 1300—1450°C after the addition of the titanium tetrachloride and aluminum trichloride is complete. PCI₃ is then added at a point where 92% of the TiCI₄ was converted to TiO₂ through a similar annular ring in sufficient quantity to provide 0.25% P₂O₅ on the titanium dioxide. The PCI₃ addition was followed by scrub solids before the reaction stream exited the reactor into cooling ducts. The reaction stream with the scrub solids was cooled. The reaction produced pigmentary size 100% rutile TiO₂.

Scrub solids are rutile TiO_2 of granular 20—40 mesh, 420 to 850 μ m (U.S.S.) size that has been calcined and was used to clean the walls of the reactor.

Comparative Example A

Rutile TiO₂ was prepared by the process of Example 1 except that sufficient AiCl₃ was added to form 1% Al₂O₃ in the TiO₂ and no PCl₃ was added.

Comparative Example B

Rutile ${\rm TiO_2}$ was prepared by the process of Example 1 except that ${\rm PCl_3}$ was added with the ${\rm TiCl_4}$ and ${\rm AlCl_3}$ and the amount of ${\rm AlCl_3}$ and ${\rm PCl_3}$ was sufficient to form 1% ${\rm Al_2O_3}$ and 0.25% ${\rm P_2O_5}$ respectively in the ${\rm TiO_2}$.

Comparative Example C

Rutile TiO_2 was prepared by the process of Example 1 except that sufficient $AlCl_3$ was added to form 1.5% Al_2O_3 and sufficient PCl_3 was added with the $AlCl_3$ to form 0.25% P_2O_5 .

45 Example 2

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Rutile ${\rm TiO_2}$ was prepared by the process of Example 1 except that sufficient ${\rm AlCl_3}$ and ${\rm PCl_3}$ was added to form 1% ${\rm Al_2O_3}$ and 0.57% ${\rm P_2O_5}$ respectively.

Example 3

The TiO₂ prepared by Examples 1 and 2 and Comparative Examples A, B and C was made into a rutile pigment slurry by the process described below and the data obtained is shown in the table that follows:

682 kg of $\rm H_2O$ were added to a grind tank. Add 10.9 kg of powdered tetrapotassium pyrophosphate and 16.4 kg of liquid 2-amino-2-methyl-1-propanol (AMP) were added to the $\rm H_2O$ and stirred until dissolved. 2730 kg of $\rm TiO_2$ prepared as described above were added over a period of 20 minutes to form a slurry. The slurry (80% solids) was ground for 30 minutes. The slurry contents were diluted to ~72% by adding 409 kg of $\rm H_2O$. The slurry was screened to remove grit. Samples were evaluated for optical value (blue green brightness) in a typical board coating formula.

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Board coating evaluation

	Example no.	% solids	Rutile	– Viscosity	Optical value	
5					Blue	Green
	Comparative Example A	72.5	99	1200	85	85
	Comparative Example B	72.4	95	600	102	102
	Comparative Example C	72.5	9899	600	103	101
10	1	71.9	99	630	102	101
	2	72.2	99	460	99	97

Example 4

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Evaluation in enamel grade pigment

The process described in Example 1 was followed except that sufficient PCl3 and AlCl3 was added to form the percent P₂O₅ and percent Al₂O₃ shown below to prepare TiO₂. From this process, 4000 grams of pigment was placed in 10 liters of water and the slurry that resulted was heated to 60°C. Fifty percent NaOH was added to bring the pH to 9.0. Three hundred and twenty cc of a sodium aluminate solution (375 g Al₂O₃/liter) and enough 20% HCl solution to maintain the pH at 9.0 was added. The pH was adjusted to 8.2 with 20% HCl. The slurry was digested for 30 minutes at 60°C, filtered, washed until the resistance of a standard sample was 7000 ohms and dried at 140°C for 48 hours. The dry powder was divided into four equal parts and ground in a fluid energy mill at rates of 350 g/min, 650 g/min, 1100 g/min and 2200 g/min. The pigment samples are evaluated in a high gloss alkyd enamel.

Alkyd enamel evaluation

	Sample	Rate	Gloss	
30	Enamel grade	650 g/min	79	
	0.25% P ₂ O ₅	1100 g/min	79	
	1.0% Al ₂ O ₃	2200 g/min	75	
35	Enamel grade	650 g/min	79	
	0.46% P ₂ O ₅	1100 g/min	78	
	1.0% Al ₂ O ₃	2200 g/min	77	

Example 5

Evaluation in plastic grade

The process of Example 1 was followed except that sufficient PCI₃ and AICI₃ was added to form the P₂O₅ and Al₂O₃ shown below to prepare TiO₂. Four thousand grams of this TiO₂ pigment were dispersed in 2000 ml of H₂O and diluted to 10,000 ml of solution by adding H₂O. The contents were stirred and heated to 60°C. Thirty-eight ml of a sodium aluminate solution were added. (341 g Al₂O₃/liter.) The pH was adjusted to 8.0 with hydrochloric acid. The mixture was cured at 60°C for 1/2 hour, filtered, washed to 7000 ohms and dried about 48 hours at 140°C. It was then screened through a 10 mesh screen and treated with a grinding aid and ground in a fluid energy mill.

Samples were also prepared by scaling the laboratory procedure that follows up to 50 tons. Samples were evaluated in polyethylene dispersed in the conventional manner.

Polyethylene evaluation

<i>5</i> 0	Polyethylene evaluation					
		Brightness	Yellow index			
55	Lab sample 0.25% P ₂ O ₅ , 1% Al ₂ O ₃ Plant sample 0.25% P ₂ O ₅ , 1% Al ₂ O ₃ Plant sample 0.25% P ₂ O ₅ , 1% Al ₂ O ₃	93.8 94.6 94.7	3.3 3.0 2.7			

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Evaluation in emulsion flat grades

The procedure of Example 1 was followed except that sufficient PCI₃ and AICI₃ was added to form

the percent P₂O₅ and percent Al₂O₃ shown below to prepare TiO₂.

Three thousand grams of this TiO₂ was placed in 10 liters of water and the slurry that resulted was heated to 70°C and 30 ml of a 20% hydrochloric acid added. Five hundred and thirty-eight ml of a sodium silicate solution (390 g SiO₂/liter) were added while maintaining the pH below 7.0 with 20% hydrochloric acid. The pH was adjusted to 7.5—8.0 with 50% NaOH solution. The slurry was digested

at 70° C for 1/2 hour. Five hundred cc of a sodium aluminate solution (360 g Al₂O₃/liter) were added while holding the pH between 7.5 and 8.0 with 20% hydrochloric acid. The slurry was digested at 70°C for 1/2 hour, filtered, washed to 7000 ohms and dried at 140°C for 48 hours. It was then ground in a fluid energy mill. The samples were evaluated in interior emulsion flat paints.

Evaluation Emulsion flat hiding

				v			
10		Interior emulsion test formula			Interior emulsion test formula		
15	Sample	0.3 kg TiO ₂ /kg 48 PVC			0.2 kg TiO ₂ /kg 55 PVC		
		HP	HPO	Stain	HP	НРО	Stain
13	Flat emulsion grade lab produced 0.25% P ₂ O ₅ 1.00% Al ₂ O ₂	120	63.0	cons ⁻	112		vvsl ⁻

The symbols in the Table have the following significance:— HP=hiding power (dry or flat), HPO=hiding power oiled, vvsl=every slightly poorer and cons=considerably poorer.

Industrial applicability

The process of this invention produces an essentially 100% rutile TiO₂ with less metallic corrosion in the oxidation reactor than when PCl₃ is added with TiCl₄ and AlCl₃. The 100% rutile TiO₂ made into a slurry for paper or board application displays superior optical values and lower slurry viscosities. The 100% rutile TiO₂ from oxidation is wet treated, filtered, washed, dried and fluid energy milled to form a dry TiO₂ for plastics pigmentation and for paints.

Claims

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- 1. A process for the manufacture of TiO_2 essentially in the rutile form by reacting $TiCl_4$ and oxygen or an oxygen containing gas in a reaction chamber in the presence of $AlCl_3$ and PCl_3 characterised in that the $AlCl_3$ and PCl_3 are separately introduced in an amount which is such as to provide from 0.1 to 0.5% by weight P_2O_5 and from 0.1 to 1.5% by weight Al_2O_3 , calculated on the weight of the final TiO_2 pigment and in that the PCl_3 is added after the $AlCl_3$ addition and at a stage in the process where $TiCl_4$ is at least 80% converted to TiO_2 .
- 2. A process for preparing titanium dioxide in essentially rutile form wherein titanium tetrachloride is reacted with oxygen in a reaction chamber characterised in that the reaction is effected in the presence of sufficient aluminum trichloride to provide from 0.1% to 1.5% by weight Al_2O_3 in the titanium dioxide and in the presence of sufficient PCl_3 to provide from 0.1% to 0.5% by weight P_2O_5 in the titanium dioxide, the PCl_3 being introduced into the reaction chamber so as to contact the reaction mixture subsequent to contact thereof with aluminum trichloride and so that the reaction mixture with which it is brought into contact has undergone at least 80% by weight conversion of titanium tetrachloride to titanium dioxide.
- 3. A process for preparing titanium dioxide in essentially rutile form wherein a mixture of titanium tetrachloride and aluminum trichloride is introduced into a tubular reactor, characterised in that the mixture contains said aluminum trichloride in an amount sufficient to provide from 0.1% to 1.5% by weight Al₂O₃ in the rutile product, said mixture is subjected to oxidation reaction with oxygen whilst displacing said mixture axially further from the point of introduction thereof to the reactor, PCl₃ is introduced into the reactor at a point downstream of said point of introduction at which at least 80% by weight titanium tetrachloride has been converted, the amount of PCl₃ introduced being such as to provide from 0.1% to 0.5% by weight P₂O₅ in the rutile product and further oxidation of titanium tetrachloride is effected in the presence of said PCl₃.
 - 4. A process as claimed in any one of Claims 1 to 3 wherein the oxygen is in the form of essentially pure oxygen or a gas containing free molecular oxygen.
 - 5. A process as claimed in any preceding claim wherein the amount of PCl_3 is sufficient to form 0.1 to 0.3% by weight P_2O_5 .
 - 6. A process as claimed in any preceding claim wherein the TiCl₄ is 88 to 98 wt.% converted to TiO₂ at the point of PCl₃ introduction.
- 7. A process as claimed in Claim 6 wherein the $TiCl_4$ is 90 to 94 wt.% converted to TiO_2 .

 8. Titanium dioxide pigment in which at least 99% is in the rutile form and which contains 0.1 to 0.3% by weight P_2O_5 and 0.1 to 1.5% Al_2O_3 , said pigment having been produced by the process claimed in any one of the preceding claims.

Patentansprüche

1. Verfahren zur Herstellung von TiO2 in im wesentlichen Rutilform, wobei TiCl4 und Sauerstoff oder ein sauerstoffhaltiges Gas in Gegenwart von AICl₃ und PCl₃ in einer Reaktionskammer reagieren, dadurch gekennzeichnet, dass AICl₃ und PCl₃ getrennt in einem Betrag, der 0.1 bis 0.5 Gew.-% P₂O₅ und 0.1 bis 1.5 Gew.-% Al₂O₃, bezogen auf das Gewicht des endlichen TiO₂—Pigment, versieht, eingeleitet werden, und dass nach dem AlCl₃-Zusatz und bei einer Verfahrenstufe worin sich mindestens 80% des TiCl₄ in TiO₂ umgewandelt PCl₃ zugesetzt wird.

2. Verfahren zur Vorbereitung von Titandioxyd, in im wesentlichen Rutilform, wobei man

10 Tetrachlortitan mit Sauerstoff in einer Reaktionskammer reagieren lässt, dadurch gekennzeichnet, dass die Reaktion in Gegenwart von Trichloraluminium stattfindet das anwesend in einem Betrag ist der gross genug ist um 0.1 bis 0.5 Gew.-% P205 im Titandioxyd vorzusehen, wobei PCI3 in die Reaktionkammer eigeleitet wird so dass wenn mindestens eine 80 Gew.-% Umwandlung von Tetrachlortitan in

Titandioxyd stattgefunden hat, wird PCI₃ mit dem Reaktionsgemisch kontaktiert.

3. Verfahren zur Vorbereitung von Titandioxyd in im wesentlichen Rutilform, wobei ein Tetrachlortitan-Aluminiumtrichlorid-Gemisch in ein röhrenförmiges Reaktionsgefäss eingeleitet wird, dadurch gekennzeichnet, dass das Gemisch einen Aluminiumtrichlord-Gehalt aufweist der gross genug ist um 0.1 bis 1.5 Gew.-% Al₂O₃ im Rutilprodukt vorzusehen, dass das genannte Gemisch, während seiner weiteren achsialen Entfernung von dem Punkt wo es in das Reaktionsefäss eingeleitet wird, mit Sauerstoff oxydiert ist, dass, an einer Stelle hinter dem gegannten Einleitungspunkt wo mindestens 80 Gew.-% Tetrachlortitan umgewandelt wurde, PCI₃ in das Reaktionsgefäss eingeleitet wird, wobei der eingeleitete PCl₃-Betrag zur Versehung von 0.1 bis 0.5 Gew-% P₂O₅ im Rutilprodukt genügt, und dass weitere Oxydation des Tetrachlortitans in Gegenwart des genannten PCI₃ stattfindet.

4. Verfahren nach einem der Ansprüche 1 bis 3, wobei der Sauerstoff als im wesentlichen reiner

Sauerstoff oder als ein Gas mit freiem Molekularsauerstoff anwesend ist.

5. Verfahren nach einem der vorangehenden Ansprüche wobei der PCl₃-Gehalt zur Formung von 0.1 bis 0.3 Gew.-% P2O5 gegügt.

6. Verfahren nach einem der vorangehenden Ansprüche wobei am Einleitungspunkt des PCI₃ 88

bis 98 Gew.-% TiCl4 in TiO2 umgewandelt wird.

7. Verfahren nach Anspruch 6, wobei 90 bis 94 Gew.-% TiCl, in TiO, umgewandelt wird.

8. Titandioxyd-Pigment in dem mindestens 90% in Rutilform ist und das 0.1 bis 0.3 Gew.-% P2Os und 0.1 bis 1.5% Al₂O₃ enthält, welches Pigment nach dem Verfahren nach einem der vorangehenden Ansprüche hergestellt worden ist.

Revendications

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1. Procédé pour la production de TiO₂, essentiellement en forme rutile, par la réaction de TiCl₄ et de l'oxygène, ou d'un gaz contenant de l'oxygène dans une enceinte de réaction en presence d'AlCl₃ et de PCl₃, charactérisé en ce que l'AlCl₃ et le PCl₃ sont introduits séparément en une quantite telle qu'elle fournit 0,1 à 0,5% par poids P₂O₅ et 1,0 à 1,5% par poids Al₂O₃, basé sur le poids du pigment Al₂O₃ finalement obtenu, et en ce qu'on ajoute le PCl₃ après avoir ajouté l'AlCl₃ et à un etage du procédé où au moins 80% du TiCl, est converti en TiO2.

2. Procédé pour la préparation du dioxyde de titane essentiellement en form rutile, dans lequel procédé on fait reagir du tétrachlorure de titane avec de l'oxygène dans une enceinte de réaction, caractérisé en ce que la réaction a lieu en presence d'une quantité de trichlorure d'aluminium telle qu'elle fournit 0,1 à 1,5% par poids Al₂O₃ dans le dioxyde de titane, et en presence d'une quantité de PCI₃ telle qu'elle fournit 0,1 à 0,5% par poids P₂O₅ dans le dioxyde de titane, le PCI₃ étant introduit dans l'enceinte de réaction afin de contacter le mélange reactionnel après que le mélange a été contacté par le trichlorure d'aluminium et afin d'amener le PCI3 en contact avec le mélange réactionnel quand au moins 80% par poids de tétrachlorure de titane a été converti en dioxyde de titane.

3. Procédé pour la préparation du dioxyde de titane essentiellement en forme rutile, dans lequel procédé un mélange de tétrachlorure de titane et trichlorure d'aluminium est introduit dans une enceinte de réaction tubulaire, lequel procédé est caractérisé en ce que le mélange comprend une quantité de trichlorure d'aluminium telle qu'elle fournit 0,1% à 1,5% par poids Al₂O₃ dans le produit rutile, en ce que ledit mélange subit une réaction oxydante par de l'oxygène pendant le déplacement axial dudit mélange à partir du lieu où il est introduit dans l'enceinte de réaction, en ce que du PCI3 est introduit dans l'enceinte à un lieu qui se trouve en aval dudit lieu d'introduction où au moins 80% par poids de tétrachlorure de titane a été converti, et en ce que la quantité de PCl₃ qu'on a introduite est telle qu'on obtient 0,1 à 0,5% par poids de P2O5 dans le produit rutile et que l'oxydation additionnelle du tétrachlorure de titane a lieu en présence dudit PCI_a.

4. Procédé selon l'une des revendications 1 à 3, dans lequel l'oxygène est formé par de l'oxygène essentiellement pur ou par un gaz qui contient de l'oxygène moléculaire libre.

5. Procédé selon l'une des revendications précédentes, dans lequel la quantité de PCl₃ suffit à former 0,1 à 0,3% par poids de P₂O₅.

6. Procédé selon l'une des revendications précédentes, dans lequel 88 à 98% par poids du TiCl₄

est converti en TiO₂ au lieu où on introduit le PCl₃.

7. Procédé selon la revendication 6, dans lequel 90 à 94% par poids du TiCl₄ est converti en TiO₂.

8. Pigment en dioxyde de titane dans lequel au moins 99% est en forme rutile et qui comprend 0,1 à 0,3% par poids de P₂O₅ et 0,1 à 1,5% par poids d'Al₂O₃, lequel pigment a été produit par le procédé selon l'une des revendications précédentes.